

**EE105**  
**Microelectronic Devices and Circuits**  
**Frequency Response**

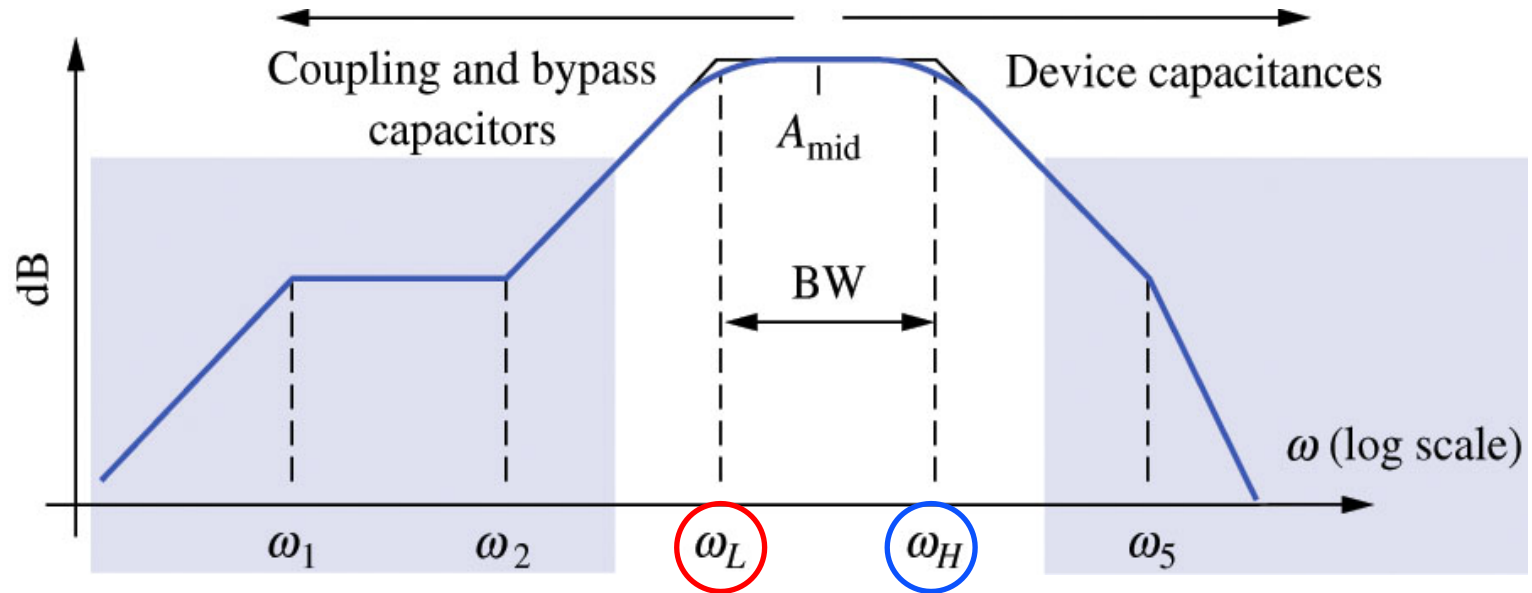
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# Amplifier Frequency Response: Lower and Upper Cutoff Frequency



- Midband gain  $A_{mid}$  and upper and lower cutoff frequencies  $\omega_H$  and  $\omega_L$  that define bandwidth of an amplifier are often of more interest than the complete transfer function
- Coupling and bypass capacitors ( $\sim \mu\text{F}$ ) determine  $\omega_L$
- Transistor (and stray) capacitances ( $\sim \text{pF}$ ) determine  $\omega_H$

# Lower Cutoff Frequency ( $\omega_L$ ) Approximation: Short-Circuit Time Constant (SCTC) Method

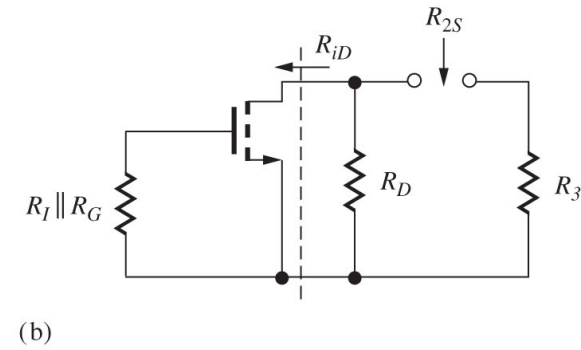
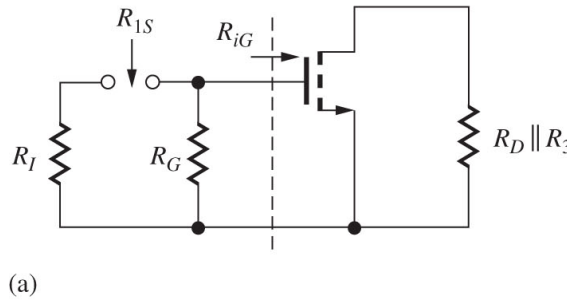
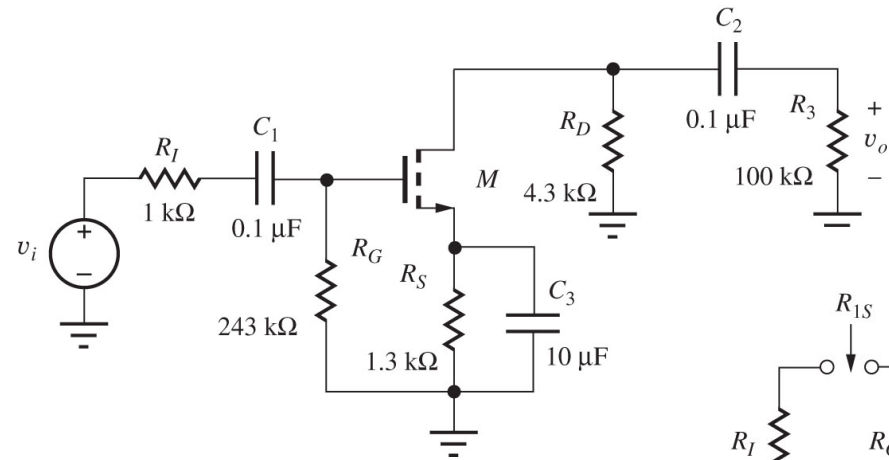
1. Identify all coupling and bypass capacitors
2. Pick one capacitor ( $C_i$ ) at a time, replace all others with short circuits
3. Replace independent voltage source with *short*, and independent current source with *open*
4. Calculate the resistance ( $R_{iS}$ ) in parallel with  $C_i$
5. Calculate the time constant,  $\frac{1}{R_{iS}C_i}$
6. Repeat this for each of the  $n$  capacitor
7. The low cut-off frequency can be approximated by

$$\omega_L \cong \sum_{i=1}^n \frac{1}{R_{iS}C_i}$$

Note: this is an approximation. The real low cut-off is slightly lower



# Lower Cutoff Frequency ( $\omega_L$ ) Using SCTC Method for CS Amplifier

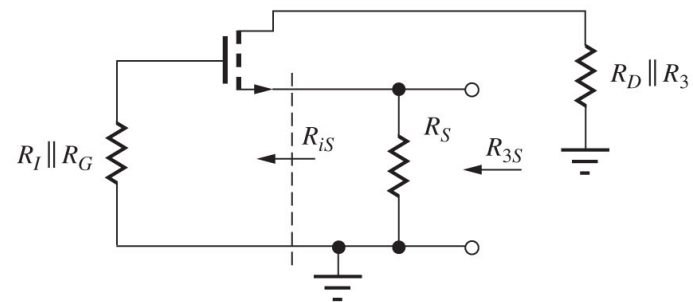


SCTC Method:

$$f_L \cong \frac{1}{2\pi} \sum_{i=1}^n \frac{1}{R_{iS} C_i}$$

For the Common-Source Amplifier:

$$f_L \cong \frac{1}{2\pi} \left( \frac{1}{R_{1S} C_1} + \frac{1}{R_{2S} C_2} + \frac{1}{R_{3S} C_3} \right)$$



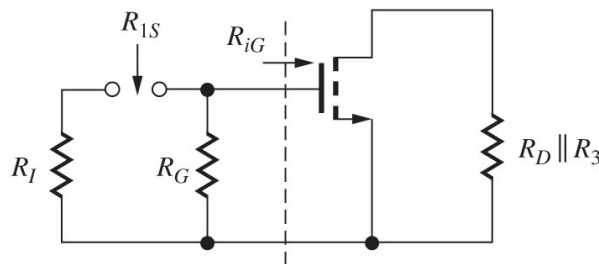
# Lower Cutoff Frequency ( $\omega_L$ ) Using SCTC Method for CS Amplifier

Using the SCTC method:

$$f_L \cong \frac{1}{2\pi} \left( \frac{1}{R_{1S}C_1} + \frac{1}{R_{2S}C_2} + \frac{1}{R_{3S}C_3} \right)$$

For  $C_1$ :

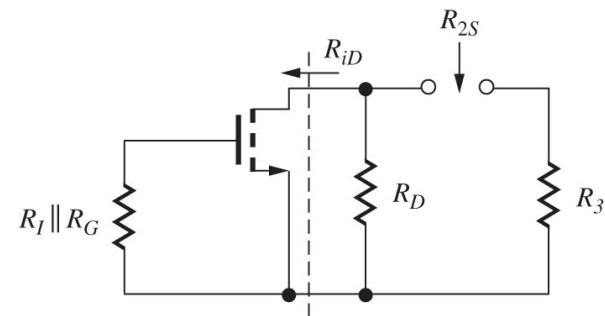
$$R_{1S} = R_I + (R_G \parallel R_{iG}) = R_I + R_G$$



(a)

For  $C_2$ :

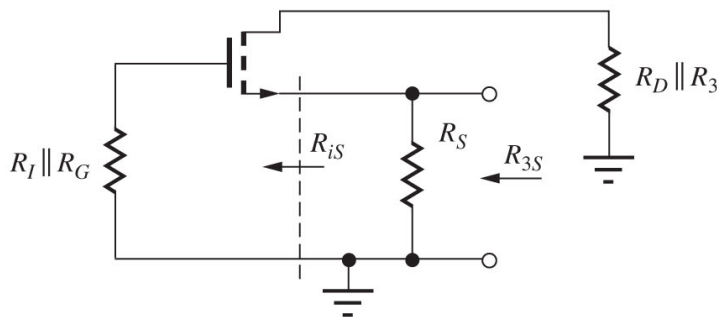
$$R_{3S} = R_3 + (R_D \parallel R_{iD}) = R_3 + (R_D \parallel r_o)$$



(b)

For  $C_3$ :

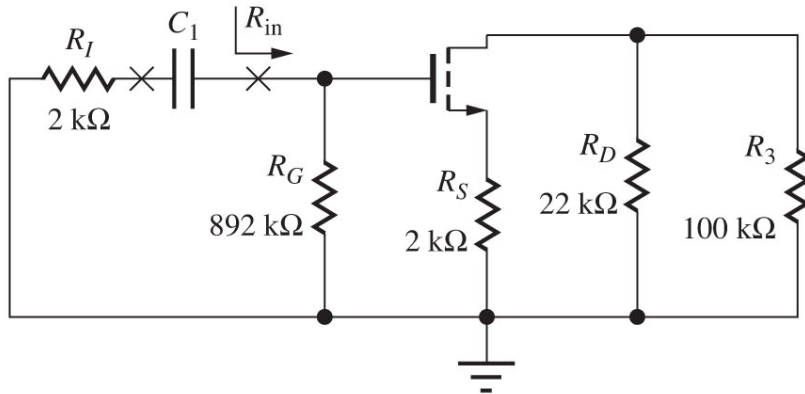
$$R_{2S} = R_S \parallel R_{iS} = R_S \parallel \frac{1}{g_m}$$



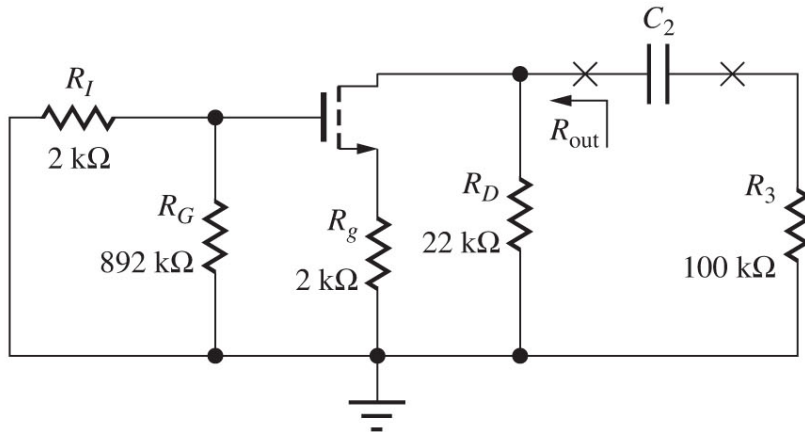
# Design: How Do We Choose the Coupling and Bypass Capacitor Values?

- Since the impedance of a capacitor increases with decreasing frequency, coupling/bypass capacitors reduce amplifier gain at low frequencies.
- To choose capacitor values, the short-circuit time constant (SCTC) method is used: each capacitor is considered separately with all other capacitors replaced by short circuits.
- To be able to neglect a capacitor at a given frequency, the magnitude of the capacitor's impedance must be much smaller than the equivalent resistance appearing at its terminals at that frequency

# Coupling and Bypass Capacitor Design Common-Source Amplifiers



(b)



For the C-S Amplifier:

$$R_{in} = R_G \parallel R_{in}^{CS} \quad R_{out} = R_D \parallel R_{out}^{CS}$$

For coupling capacitor  $C_1$  :

$$C_1 \gg \frac{1}{\omega(R_I + R_{in})}$$

For coupling capacitor  $C_3$  :

$$C_2 \gg \frac{1}{\omega(R_3 + R_{out})}$$

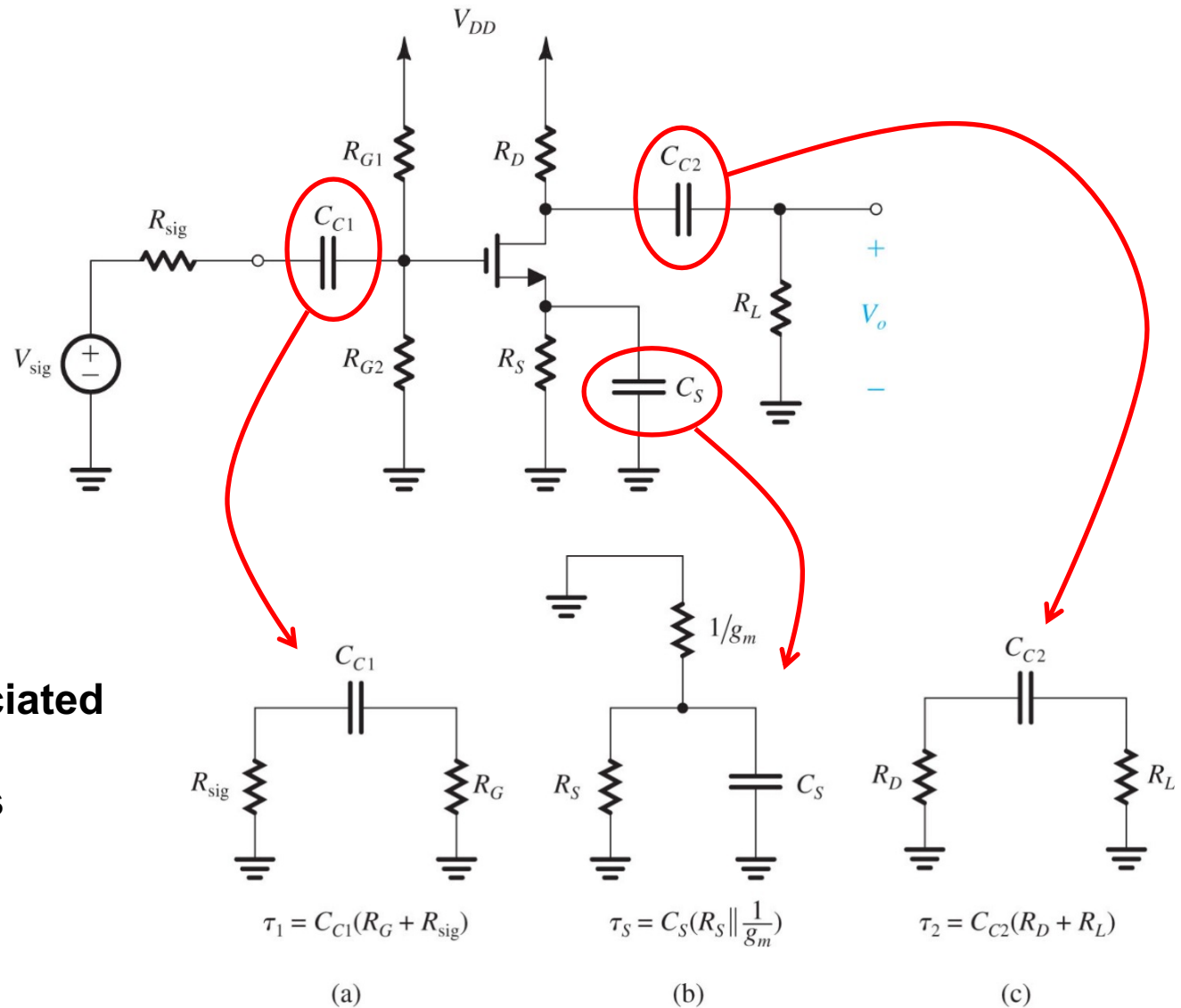
# Lower Cutoff Frequency $f_L$

## Dominant Pole Design

- Instead of having the lower cutoff frequency set by the interaction of several poles, it can be set by the pole associated with just one of the capacitors. The other capacitors are then chosen to have their pole frequencies much below  $f_L$ .
- The capacitor associated with the emitter or source part of the circuit tends to be the largest due to low resistance presented by emitter or source terminal of transistor and is commonly used to set  $f_L$ .
- Values of other capacitors are increased by a factor of 10 to push their corresponding poles to much lower frequencies.



# Capacitively Coupled CS Amplifier



Find the pole frequency associated with each coupling/bypass capacitor:

# Low Frequency Response

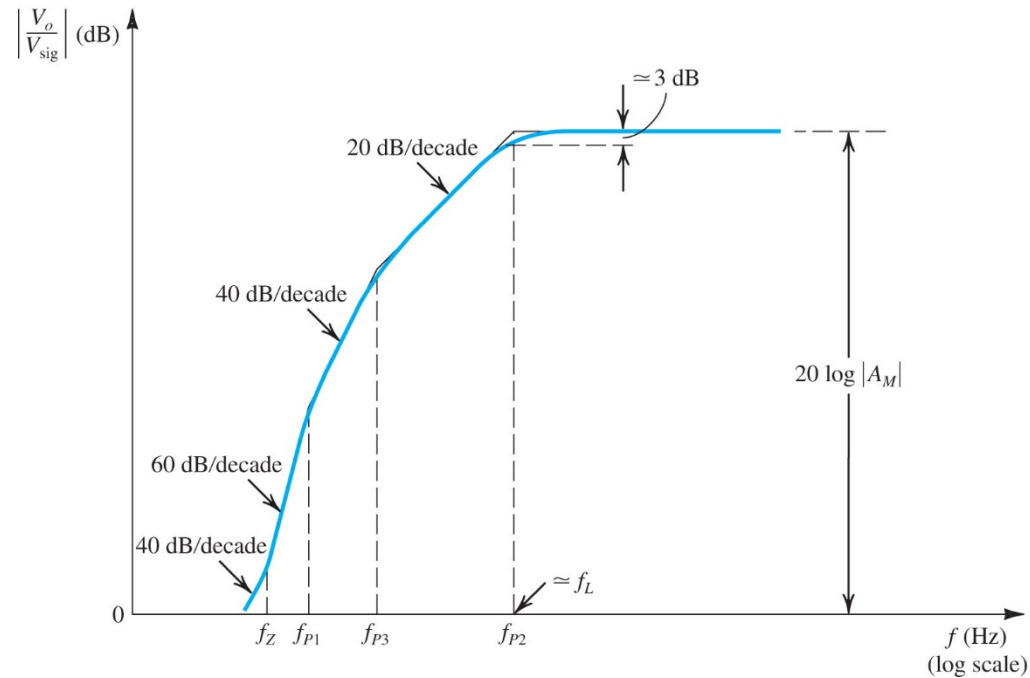
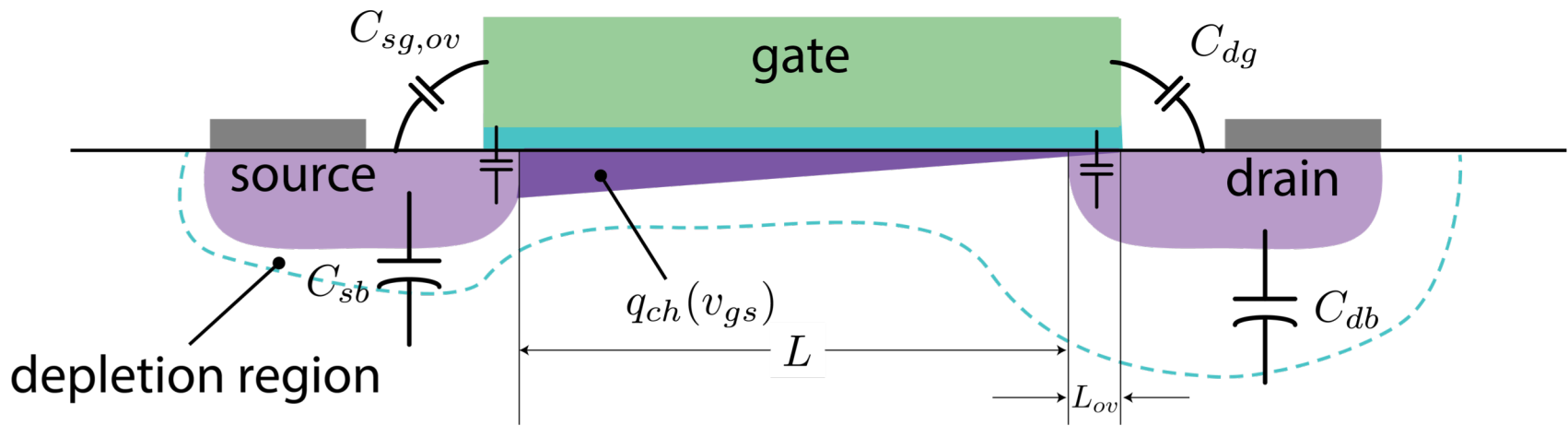


Figure 10.7 Sketch of the low-frequency magnitude response of a CS amplifier for which the three pole frequencies are sufficiently separated for their effects to appear distinct.

# High Frequency Response

# Capacitors in MOS Device



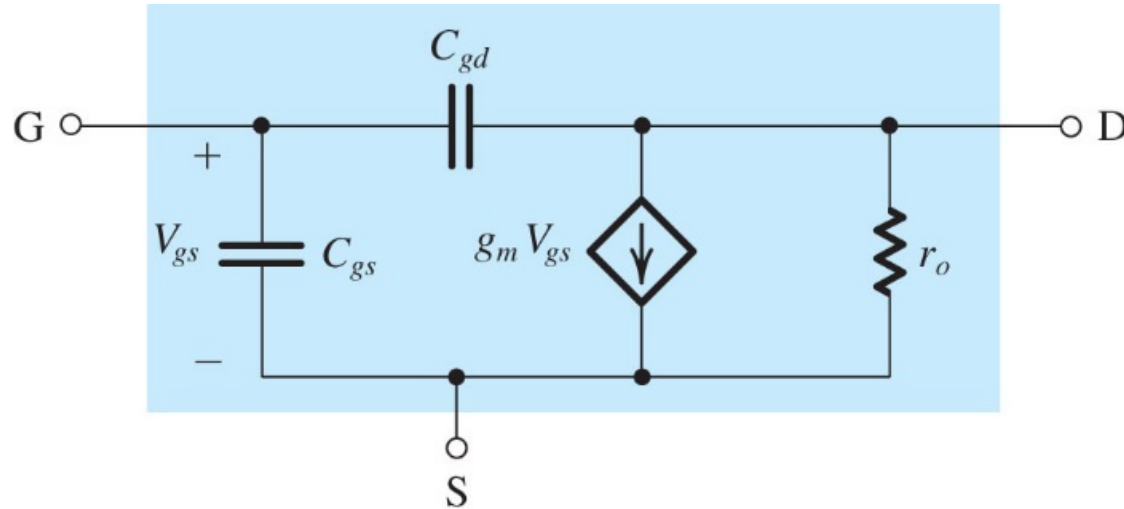
$$C_{gs} = (2/3)WLC_{ox} + C_{ov}$$

$$C_{gd} = C_{ov}$$

$$C_{sb} = C_{jsb} (\text{area} + \text{perimeter}) \text{ junction}$$

$$C_{db} = C_{jdb} (\text{area} + \text{perimeter}) \text{ junction}$$

# (Simplified) High-Frequency Equivalent-Circuit Model for MOSFET



Capacitances between source/body,  $C_{sb}$ , and between drain/body,  $C_{db}$ , are neglected